Partitioning Field Evapotranspiration Fluxes by Using Stable Oxygen Isotope during Different Maize Growth Stages

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Abstract

Field evapotranspiration is an important component in Soil Plant Atmosphere Continuum (SPAC), and it is comprised of plant transpiration and soil evaporation. However, the two components of which is difficult to partition. A field experiment was conducted in the Northern China to determine the maize transpiration and soil

evaporation during a maize growth period using stable oxygen isotope. A water balance model in field was used to estimate the field evapotranspiration. Maize transpiration and soil evaporation were estimated during the five typical growth stages of seedling, jointing, booting, tasseling, and filling-mature, respectively. The results showed that total field evapotranspiration during the whole maize growth period was 481.8 mm and distributed in the five growth stages were 122.7, 81.9, 82.5, 71.5 and 123.2 mm, respectively, and the fraction of maize transpiration in field evapotranspiration in the five growth stages were 11.8%, 65.0%, 78.3%, 81.8%, and 50.02%, respectively.

Keywords: Field evapotranspiration, Field water balance model, Maize transpiration, Soil evaporation, Isotope mass balance model

Abbreviations: SPAC, Soil Plant Atmosphere Continuum; *ET*, evapotranspiration; *T*, plant transpiration; *E*, soil evaporation; δ^{18} O, oxygen isotopic composition; *q*, soil water flow flux; *K*, unsaturated hydraulic conductivity; φ , soil water potential; *D*, distance; *K_s*, saturated hydraulic conductivity; *S*, saturation; θ , soil volumetric water content; θ_r , soil residual volumetric water content; θ_s , soil saturated volumetric water content; *F_E*, the fraction of soil evaporation in the field evapotranspiration; *F_T*, the fraction of plant transpiration in the field evapotranspiration; *K_a*, atmospheric relative humidity; α_{K} , kinetic fractionation factor; α_{eq} , equilibrium fractionation factor; *T*, soil temperature; *m* mass of water (presented as mm); *P*, precipitation; *S_c*, field moisture capacity; *C*, the concentrations of the H₂O.

1. Introduction

Water cycle in Soil Plant Atmosphere Continuum (SPAC) has been the popular research topic since Philip firstly advised the conception of SPAC in 1966 (Philip, 1966). In order to understand the water sources or sinks in SPAC and mass balance mechanism in agroecosystem, one of the key problems is to realize the water transporting and transitions in field. Field evapotranspiration is an important component in SPAC, which is composed by plant transpiration and soil evaporation and is difficult to estimate (Yepez et al., 2003).

Micrometeorologic methods such as Bowen ratio model and eddy covariance had been used to calculated evapotranspiration (Williams et al., 2004; Wilson et al., 2001; Paco et al., 2006; Sun et al., 2008), but usually limited by much parameters and complicated calculation processes. Large-scale weighing lysimeter made direct measurements of water loss from growing crop and the soil surface around crop (Vaughan et al., 2007), and thus, the measurement was exact in some extent, but it has poor spatial representation (Yepez et al., 2003; Jarvis, 1995). Water balance model have been widely applied to determined field evapotranspiration (Steinwand et al., 2006), while exact and precise methods are needed for obtaining the components of the model such as precipitation and infiltration or capillary rise.

Crop transpiration was significant for determining water use efficiency in field (Allen et al., 2003), and which could be measured precisely by portable photosynthesis system, but the measurement results only represented the instantaneous state of the leaf level. Therefore, partition plant transpiration and soil evaporation in field from evapotranspiration was necessary and difficult (Baldocchi et al., 1988; Scott et al., 2003; Yepez et al., 2003). Although evaporation from soil surface in some greenhouse experiments could be inhibited by enclosing the pots (Li, 1999; Zhao et al., 2004), soil evaporation was unavoidable in field. Water vapor evaporated from soil surfaces was strongly fractionated and its isotope composition was significant difference from isotope composition of leaf water (Flanagan et al., 1991); Therefore, an isotope mass balance model could be used to partition evapotranspiration into its components and was presented as follows(Yakir and Sternberg, 2000):

$$ET = E + T \tag{1}$$

$$ET\delta_{ET}^{18}O = E\delta_{E}^{18}O + T\delta_{T}^{18}O$$
⁽²⁾

where *ET* was evapotranspiration, *T* was maize transpiration, and *E* was soil evaporation. δ_{ET}^{18} O, δ_{T}^{18} O and δ_{E}^{18} O were the oxygen isotopic composition of evapotranspiration, transpiration, and evaporation water, respectively.

The model had been widely applied in the water flux studies in forest (Moreira et al., 1997), orchard (Williams et al., 2004), grassland (Ferretti et al., 2003), while few had been conducted in field crops due to the accurate values of ET, δ_{ET}^{18} O, δ_{T}^{18} O and δ_{E}^{18} O in the model were difficult to obtain in field crops.

Huang-Huai-Hai Plain, located in northern China, is an important grain production base that accounts for about 30% of the grain produced nationally in China. The main crop grown in this area is maize. It is important to evaluate water consumed in the field and partition the field evapotranspiration into maize transpiration and soil evaporation. Such efforts not only contribute to our understanding of the water cycle in SPAC of agroecosystem, but also provide theoretical guidance for water-saving techniques in agriculture. Therefore, the main objectives

of this study were to (1) estimate field evapotranspiration during different growth stages of maize using a field water balance model; (2) obtain the parameters (δ_{ET}^{18} O, δ_{T}^{18} O and δ_{E}^{18} O) of the isotope mass balance model and partition field evapotranspiration into maize transpiration and soil evaporation during different growth stages.

2. Materials and methods

2.1 Study site description

Field experiments were conducted at the Agro-ecological Experimental Station of the Chinese Academy of Sciences in Fengqiu, Henan Province, located in the Huang-Huai-Hai Plain in north China (35°01'N, 114°24'E). The study area is located in a temperate zone and has a semi-humid monsoon climate. The annual precipitation in the area is approximately 615 mm, 60–90% of which occurs from May to October, and the average annual temperature in the area is 13.9 °C. The soil type is fluvo-aquic soil and the profiles generally consist of three layers, with sandy loam being present at depths of 0-30 cm, silty clay being present at 30-60 cm, and sandy loam being present at 60-170 cm. Some basic physical and chemical properties of the soil are listed in Table 1. All soil properties were determined following standard methods as indicated in the footnote of Table 1.

2.2 Field experimental design

Experimental plots were established in the station with three replicates. Each plot measured 8×6 m and was separated by concrete walls that were inserted into the soil to a depth of 0.8 m, with 0.2 m remaining above the soil surface. Maize was seeded on June 5, 2007 and harvested on September 12, 2007. According to local practice, 190 kg ha⁻¹ N (as urea), 80 kg ha⁻¹ P₂O₅ (as [Ca (H₂PO₄)₂] with 46% P₂O₅) and 200 kg ha⁻¹ K₂O (as K₂SO4 with 50% K₂O) were applied. Nitrogen fertilizer was split broadcast, with 40% being applied as basal fertilizer before seeding and the rest being applied at booting. The other fertilizers mentioned above were applied completely as basal fertilizers. The growth stages of seedling, jointing, booting, tasseling, and filling were started on June 14, July 12, July 22, August 2 and August 20, respectively. The variety of maize grown was Zhengdan 958 and its population was about 62,500 plants per hectare.

A PVC (Polyvinyl Chloride) tube with a diameter of 5 cm was installed in the center of one plot to a depth of 8 m and used for groundwater monitoring every 5 days. A plastic cap was used to cover the tube after observation to avoid contamination. Soil volumetric water content was measured at 17 depths (every 10 cm from soil surface to 170 cm depth) at 5 days intervals in each plot using neutron soil moisture probe (CNC 503, produced by Beijing Chaoneng Technology Co. LTD). Soil water potential was measured by Portable SM-1 type of soil water potentiometer (Xin et al., 2007) at the five depths (20, 40, 80, 170 and 190 cm) for every 5 days. In addition, both of soil volumetric water content and soil water potential were measured again when rainfall events happened. Two ceramic suction cups were installed in each plot at the depths of 20 and 40 cm to extract soil water of different layers. Finally, meteorological data was obtained from a weather station located 10 meters east of the study field on a daily basis.

2.3 Water balance model in the field

A field water balance model was used to calculate field evapotranspiration (ET):

ET = Precipitation - Soil water variety- Runoff - Crop interception- Infiltration + Capillary rise (3)

where precipitation was obtained from the weather station; soil water variety was calculated from the observation results of soil volumetric water content; runoff and crop interception were ignored; and infiltration or capillary rise were estimated through soil water flow flux (q) and water flow direction (up or down), which were determined by water potential measured by soil water potentiometer. Water flow flux q was calculated using Darcy's Law:

$$q = -K \times (d\varphi/dD) \tag{4}$$

where K was the unsaturated hydraulic conductivity which depended on soil volumetric water content or soil water potential; φ was soil water potential which was measured by portable SM-1 type of soil water potentiometer; D was the distance. K was obtained through van Genuchten-Mualem model:

$$K = K_{\rm s} S^{0.5} (1 - (1 - S^{1/m})^m)^2$$
(5)

$$S = (\theta - \theta_r) / (\theta_s - \theta_r) \tag{6}$$

where K_s was saturated hydraulic conductivity; S was saturation; θ was soil volumetric water content, θ_r and θ_s were the soil residual and saturated volumetric water contents, respectively, m was a parameter relating to the shape of soil water retention curve (Li. *et al*, 2007). θ was measured by neutron soil moisture probe, θ_s was

shown in Table 1, θ_r and *m* were estimated by pedo-transfer functions as the research of Li which was conducted in the same study area (Li. *et al.* 2007).

When calculating field evapotranspiration with the water balance model, we supposed that infiltration or capillary rise water boundary was the groundwater table. If the groundwater table was deeper than 1.7 m, the boundary was fixed at 1.7 m depth.

2.4 Sampling for stable isotope analysis

During each growth stage, we installed an airtight flexible cylindrical tube in the water outlet of a dehumidifier (Super dehumidifier MDH-616A, Morii, Japan), and the tube was inserted into an airtight bottle to collect air vapor in the field. Transpired water from maize leaf was collected directly through an airproof bag which was covered around the leaves tightly as described by Yakir et al. (1993). Soil water at the surface of 20 cm and the depths of 20~40 were extracted using ceramic suction cups under -0.85 kPa after 12 hours of equilibrium in each plot. The above water samples were collected during each growth stage on June 24, July 17, July 30, August 18 and September 2, respectively. During each rain event, rainwater was collected in the field using rain gauges that contained paraffin oil (at least 2 mm) to prevent evaporation (Dodd et al., 1998). When rain events lasted for several days, the rainwater was collected every day to eliminate the potential evaporation.

All of the water samples were collected with three replication, and then transferred into airtight bottles immediately upon collection and stored in the laboratory at -20 until isotopic analysis.

2.5 Sable oxygen isotope analysis

In this study, the oxygen isotope ratios were analyzed by the CO_2 equilibration method (Scoki et al., 1999) using 2 ml water samples that were equilibrated with CO_2 overnight at 25 \cdot . The stable oxygen isotope in the treated samples were analyzed using a MAT253 isotope ratio mass spectrometer (Thermo Finnigan America).

Isotope composition is usually expressed as the molar ratio of heavier to lighter isotopes (*R*), whereas the absolute quantity of stable isotopes in nature is extremely low. For convenience, *R* is generally converted to values of δ (stable isotope composition),

$$\delta(\%) = (R \text{ (sample)} / R \text{ (standard)-1}) \times 1000$$
(7)

where *R* (sample) and *R* (standard) are the molar ratios of the heavier and lighter isotope of the sample and the standard, respectively. The standard in this study was V-SMOW (Vienna standard mean ocean water). The analytical precision was 0.1‰ and the accuracy was better than 0.1% for δ^{18} O.

2.6 Methods for obtaining parameters of isotope mass balance model

The isotope mass balance model could be expressed as:

$$\delta_{ET}^{18} \mathbf{O} = F_E \delta_{ET}^{18} \mathbf{O} + F_T \delta_T^{18} \mathbf{O}$$
(8)

$$F_E + F_T = 1 \tag{9}$$

where F_E and F_T were the fraction of soil evaporation and plant transpiration in the field evapotranspiration, respectively; the others symbols were the same as described above.

ET could be estimated through the field water balance model, $\delta_T^{18}O$ was measured from the transpired water directly (Harwood et al., 1998), $\delta_E^{18}O$ was transformed from $R_E^{18}O$ according to the Eq. (7), and $R_E^{18}O$ was calculated by the following equation (Moreira et al., 1997; Yepez et al., 2003):

$$R_{\rm E}^{18}{\rm O} = (1/\alpha_K) \times (R_{\rm S}^{18}{\rm O}/\alpha_{eq} - R_{\rm a}^{18}{\rm O} \times h)/(1-h)$$
(10)

where R_E^{18} O, R_8^{18} O, R_a^{18} O were the molar ratio of heavier to lighter isotope of evaporation water from soil surface, soil water at the evaporation surface, and air vapor, respectively; *h* was the atmospheric relative humidity and could be obtained from the weather station; α_K was the kinetic fractionation factor which depended on the differences in reaction rates and diffusion coefficients of isotope molecules in air, and would be higher values for diffusive and lower values for turbulent boundary layers (Moreira et al., 1997; Yepez et al., 2003; Yakir & Sternberg, 2000), here we selected 1.0285 for oxygen; α_{eq} was the oxygen equilibrium fractionation factor for two phases of liquid water and vapor which was the function of temperature, and could be expressed as follows (Yepez et al., 2003):

$$\alpha_{eq}^{18}\text{O} = (1.137(10^6/\text{T}^2) - 0.4156(10^3/\text{T}) - 2.0667)/1000 + 1$$
(11)

where T was the soil temperature in K.

We applied a simple isotope mass balance model in the top surface 20 cm soil to estimate the δ_{ET}^{18} O (Hsieh et al., 1998; Ferretti et al., 2003). During each growth stage:

$$m_{initial} + m_P + m_{rise} = m_{final} + m_{ET} + m_{infiltration}$$
(12)

$$\delta_{initial}^{18} O \ m_{initial} + \delta_P^{18} O \ m_P + \delta_{rise}^{18} O \ m_{rise} = \delta_{final}^{18} O \ m_{final} + \delta_{ET}^{18} O \ m_{ET} + \delta_{infiltration}^{18} O \ m_{infiltration}$$
(13)

where *m* referred to the mass of water (presented as mm) and δ^{18} O represented the oxygen isotope composition of each component. The subscripts of *initial*, *final*, *rise*, *infiltration*, *P* and *ET*, represented water in the initial soil, final soil, capillary rise, infiltration, precipitation, and evapotranspiration during each growth stage, respectively. Sampling date was determined by the maize growth stage, which was the final sampling date of the prior stage, and the initial date of the next stage.

Values of $m_{initial}$ and m_{final} were measured by neutron soil moisture probe, m_P was observed in the weather station, and m_{ET} was obtained by the water balance model (Eq.3), then m_{rise} or $m_{infiltration}$ could be obtained through equation (12). $\delta_{initial}^{18}$ O and δ_{final}^{18} O were the isotope composition of the top surface 20 cm soil water.

 δ_P^{18} O was the precipitation isotope composition which was weighted for each rainfall, if there were rainfall events more than one time in some growth stages (determined by multiplying the isotopic composition by precipitation of each time and dividing by the total precipitation), and which was expressed as follows:

$$\delta_P^{-18} \mathbf{O} = \sum (P_i \delta_{P_i}^{-18} \mathbf{O})/m_P \tag{14}$$

where P_i was the rainfall for each rainfall event and δ_P^{18} O was its isotope composition, the others symbols means were the same as mentioned above.

We assumed that the top surface 20 cm soil couldn't retain the precipitation and formed infiltration when heavy rainfall made soil water content excess field moisture capacity, and thus $\delta_{infiltration}^{18}$ O was given as:

$$\delta_{infiltration} {}^{18}\text{O} = \sum (P_j + S_j - S_c) \,\delta_{Pj} {}^{18}\text{O}/\,m_{infiltration} \tag{15}$$

where S_c was the field moisture capacity (Table 1), P_j was the rainfall for each heavy rainfall which leaded to infiltration and $\delta_{P_j}^{18}$ O was its isotope composition, S_j was the soil water content before the precipitation. Eq.(15) would only been established when the value $(P_i + S_j)$ was greater than S_c .

If the next layer water rose up to the top 20 cm, δ_{rise}^{18} O was the water in 20~40 cm depth. Substituted these parameters into equation (13) and δ_{ET}^{18} O of each growth stage could be calculated.

After we obtained δ_E^{18} O and δ_T^{18} O, and then substituted δ_E^{18} O, δ_T^{18} O and δ_{ET}^{18} O in to Eqs. (8) and (9), the fraction of transpiration in the field evapotranspiration was,

$$F_T = (\delta_E^{-18} \text{O} - \delta_E^{-18} \text{O}) / (\delta_E^{-18} \text{O} - \delta_T^{-18} \text{O})$$
(16)

3. Results and discussion

3.1 Rainfall, groundwater table, soil volumetric water content and soil water potential during different growth stages of maize

The total rainfall was 427.4 mm and the daily rainfall during the maize growth period was shown in Fig.1. The experimental station was located approximately 15 km from the Yellow River, where the groundwater table varied greatly with seasons (rain season and dry season) and the Yellow River flood season. The groundwater table gradually increased from June 14 (seedling) to August 4 (tasseling), ranging from 4.2 m to 1.09 m below the ground, while it fluctuated between 1.95 m and 0.95 m in the subsequent growth stages.

Similar to the groundwater table, the soil volumetric water content increased throughout the entire maize growth period, although it varied slightly between jointing and booting (Fig.2). The spatial distribution of the soil volumetric water content in the profile from the surface to 1.7 m was more complicated than the temporal distribution. Specifically, the soil volumetric water content increased continually from 20 cm to 80 cm over the growth period, although it showed a decrease of about 1 m depth during the seedling, jointing and booting stages. This was likely because the rainy season began in May and rain water primarily replenished the upper soil water, but did not reach below 1 m depth during the three previous growth stages. From tasseling to filling, the soil water content at depths of 20 and 40 cm was usually lower than 0.3 m³ m⁻³. Groundwater was usually greater than 1.7 m during tasseling (Fig.1), which lead to saturated soils at this depth and little variation during this period (data not shown, Fig.2 only shows the soil volumetric water content on the soil water sampling day).

The soil water potential increased continually from the time of planting and presented a wave-shape during the tasseling stage (Fig.3). From seedling to booting, the soil water potential at 20 and 40 cm depths increased slightly when compared to the potential at 80 cm depth. During tasseling and filling, the soil water potentials at depths of 20 and 40 cm were lower than at depth of 80 cm. The lowest soil water potential in seedling, jointing and booting was the interface of silt clay and sandy loam at the depth of 0.8 m (Table 1), and exhibited the highest value in 1.9 m depth from tasseling to mature (Fig.3).

3.2 Field evapotranspiration during different growth stages

The components of water balance model (evapotranspiration, precipitation, infiltration or capillary rise, and variety of soil water) were shown in Table 2, which showed that infiltration and capillary rise reached lowest in the stage of filling-mature and booting, respectively, while reached greatest during the stage of booting and filling-mature, and soil water variation fluctuated from -11.1 mm (negative sign represent the soil water decreased when compared to the prior growth stage) in booting to 19.1 mm in seedling. Field evapotranspiration was 481.8 mm, and precipitation occupied most of the field evapotranspiration during the maize growth period.

3.3 Partitioning evapotranspiration into maize transpiration and soil evaporation

Soil water sampling date and the parameters used in Eq.(10) for $\delta_{\rm E}^{18}$ O estimation were listed in Table 3. On account of water infiltration and capillary rise, the parameters used to estimated $\delta_{\rm ET}^{18}$ O with Eqs.(12) and (13)were showed in Table 4. Values of $\delta_{\rm E}^{18}$ O and $\delta_{\rm ET}^{18}$ O for each growth stage were substituted in Eqs.(8) and (9), F_T was worked out and was shown in Table 5. The ratio of maize transpiration to field evapotranspiration during the stages of seedling, jointing, booting, tasseling, and filling-mature were 11.8%, 65.0%, 78.3%, 81.5%, 50%, respectively, The maize transpiration and soil evaporation of the whole growth period were 252.4 mm and 229.4 mm, and took up 52.4% and 47.6% of the water consumed by the whole field evapotranspiration, respectively. Water consumed by transpiration distributed in the stage of seedling, jointing, booting, tasseling, and filling-mature were 14.5, 53.2, 64.6, 58.5, and 61.6 mm, respectively, accordingly, the distribution of soil evaporation in the five growth stages were 108.3, 28.7, 17.9, 13.0, and 61.6 mm, respectively.

3.4 Water dynamic in field during maize growing period

High precipitation(annual average was about 615 mm and 427.4 mm distributed in the period of maize growing), groundwater table and evapotranspiration during maize growing period leaded to water transport frequently in soil in the study area and produced obvious effect on soil water potential and soil volumetric water content.

Water flow direction in soil was determined by the soil water potential and flow from the high potential position to the low potential position. The variation of soil water potential in profile indicated that infiltration and capillary rise water were indeed existed during the maize growth period (Fig.3). Before July 29 (in booting), the groundwater table was lower than 1.7 m. The value of soil water potential gradient between 1.7 and 1.9 m depth was various and leaded to infiltration or capillary rise took place between soil and groundwater; the soil water potential at 0.8 m was lowest from June 14(in seedling) to July 29(in booting), and the water above and underside would flow to this layer, and leaded soil volumetric water content of this layer increased (Fig.2). Obviously, field evapotranspiration in this period mainly came from the soil water above 0.8 m and precipitation. From July 29(in booting) to maize mature, the soil water potential gradually increased with depth, and main water flow in soil was capillary rise (Fig.3).

Water lost in seedling was mainly from soil evaporation, and the proportion of water consumed by maize transpiration in the evapotranspiration apparently increased from seedling to tasseling, and took up most of field evapotranspiration in jointing, booting, and tasseling, then decreased from filling to mature. The similar trend was also reported by Kang et al. (2003) based on a study in a semi-arid region of northwest China (34°20'N, 108°24'E), and which could provide an indirect confirmation that the calculation results of isotope mass balance model was accurate.

3.5 Advantages of the isotope mass balance model

The estimation of the parameters δ_{ET}^{18} O in Eq. (8) was important when stable oxygen isotope was applied in water flux studies in terrestrial ecosystems. Most of present researchers used Keeling plot to estimate δ_{ET}^{18} O (Bowling *et al.* 2001; KÖhler et al., 2006), since it was founded by Keeling (1960) based on mass conservation principle during the exchange of water between two reservoirs. Application of keeling plot in a given ecosystem (such as agroecosystem) was expressed as follows:

$$C_{new} = C_a + C_{add} \tag{17}$$

$$C_{new}\delta_{new}^{18}O = C_a\delta_a^{18}O + C_{add}\delta_{add}^{18}O$$
(18)

where C_{new} , C_a and C_{add} were the concentrations of the H₂O in the given ecosystem, in the atmosphere and that added component to this ecosystem, respectively; δ_x^{18} O represented the stable oxygen isotopic composition of the component x.

Combining Eqs.(17) and (18), we got the equation (19),

$$\delta_{new}^{18} O = C_a (\delta_a^{18} O - \delta_{add}^{18} O) (1 / C_{new}) + \delta_{add}^{18} O$$
(19)

This was a linear relationship of δ_{new}^{18} O versus the inverse of its concentration with a slope of $C_a(\delta_a^{18}\text{O} - \delta_{add}^{18}\text{O})$, and an intercept at the value of $\delta_{add}^{18}\text{O}$.

There were three basic limitations when Keeling plot was applied in the studies of water flux: (1) the ecosystem consisted of only two reservoirs; (2) the isotope ratio of the added reservoir did not change during the experimental period. However, If the added ecosystem component was composed of several different sources or sinks (KÖhler et al., 2006), from Eq.(19), the Keeling plot still could be used as long as the relative contribution of each of these subcomponents remained fixed (Yakir and Sternberg, 2000); (3) A series of data of the vapor concentration (C_{new}) and its oxygen isotope composition (δ_{new}^{18} O) in the given ecosystem should present some differences during the experiment time, and thus ensured the Eq.(19) could be obtained. This condition was easy to satisfy in a closed ecosystem but was difficult to realize in an open ecosystem. Otherwise, if C_{new} and δ_{new}^{18} O varied with height and could be measured, the Keeling plot could also be used to estimate δ_{ET}^{18} O, and which was adapted well to forest ecosystem with high trees, but which was also difficult to fulfill in an agroecosystem with maize grown. Therefore, we used a simple isotope mass balance model to determine δ_{ET}^{18} O during each maize growth stages, and still considered the effect of infiltration or capillary rise, and made sure the calculated results was more exact.

4. Conclusions

In this study, an isotope mass balance model was used to partition field evapotranspiration into maize transpiration and soil evaporation during different growth stages. The methods for obtaining the parameters of δ_{ET}^{18} O, δ_T^{18} O and δ_T^{18} O could overcome the limitations of Keeling Plot which had been widely used in water flux studies in terrestrial ecosystems. And we consider the methods in this study are not only able to partition field evapotranspiration into plant transpiration and soil evaporation in agroecosystem, but also can be applied to research water cycle in other ecosystem, such as forest, grassland and desert ecosystems.

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| | | Particle size ^a /% | | | | | Field | Saturated | Saturated | |
|--------------|-----------------|-------------------------------|------|------|--|---|---|--|--|---|
| Depth /cm | Soil texture | Sand | Silt | Clay | Organic C ^b /g kg ⁻¹ | Bulk density ^c /g cm ⁻³ | Electric conductivity ^d /µS cm ⁻¹ | moisture capacity ^e /cm ³ cm ⁻³ | volumetric water content ^f /cm ³ cm ⁻³ | hydraulic conductivity ^g /mm h ⁻¹ |
| 0-30 | Sandy loam | 72.9 | 17.5 | 9.6 | 7.4 | 1.55 | 118.13 | 0.275 | 0.415 | 22.6 |
| 30-80 | Silt Clay | 47.0 | 34.5 | 18.5 | 14.3 | 1.41 | 173.67 | 0.280 | 0.475 | 19.3 |
| 80-170 | Sandy loam | 62.0 | 28.1 | 9.9 | 3.6 | 1.47 | 186.41 | 0.262 | 0.452 | 18.1 |

Table 1. Some physical and chemical properties of the soil in the study area

^aParticle size: pipette method (ISSCAS, 1978a)

^bOrganic C: dichromate method (ISSCAS, 1978b)

^cBulk density: cutting ring method (ISSCAS, 1978a)

^dElectric conductivity: 1:5 soil to water

^eField moisture capacity: cutting ring method (ISSCAS, 1978a)

^f Saturated volumetric water content: cutting ring method (ISSCAS, 1978a)

^g Saturated hydraulic conductivity: measured using a CRISO disc permeameter in the field (CRISO, 1988)

| Table 2. The components | of water balance mo | del (evapotranspiration, | , precipitation, | infiltration | or capillary | y rise, |
|----------------------------|---------------------|--------------------------|------------------|--------------|--------------|---------|
| soil water variety) during | each growth stage | | | | | - |

| Water(mm) | | Tatal (mm) | | | | |
|--------------------|------------|------------|------------------|-----------|-----------------|------------|
| | Seedling | Jointing | Booting | Tasseling | Filling-mature | Total (mm) |
| Precipitation | 127 | 70.4 | 115.3 | 61 | 53.7 | 427.4 |
| Infiltration | 5.4(0.3) | 9.3(0.5) | 42.8(2.6) | 28.4(1.4) | 2(0.1) | 87.9 |
| Capillary rise | 20.1(1.8) | 34.7(2.1) | 0 | 44.5(2.4) | 65.6(3.6) | 165.0 |
| Soil water variety | 19.1(1.2) | 14.0(1.8) | $-11.1(1.3)^{1}$ | 5.5(0.9) | $-5.9(0.8)^{a}$ | 21.66 |
| ET | 122.7(4.8) | 81.9(3.2) | 82.5(3.1) | 71.5(4.4) | 123.2(5.4) | 481.8 |

^anegative sign represent the soil water decrease; The data in the parentheses referred to the standard deviation

| Deremeters | Growth stages | | | | | | |
|----------------------------------|---------------|------------|------------|------------|----------------|--|--|
| Falameters | Seedling | Jointing | Booting | Tasseling | Filling-mature | | |
| Sampling date | June 24 | July 12 | July 30 | August 18 | September 20 | | |
| Soil temperature(°C) | 30.2(0.2) | 27.8(0.1) | 25(0.2) | 34(0.2) | 32.1(0.2) | | |
| α_K | 1.0285 | 1.0285 | 1.0285 | 1.0285 | 1.0285 | | |
| α_{eq} | 1.00893 | 1.00912 | 1.008718 | 1.00934 | 1.00879 | | |
| h(%) | 74(2) | 78(3) | 82(2) | 93(4) | 86(2) | | |
| $\delta_{ m S}^{18}{ m O}(\%)$ | -0.7(0.2) | -2.4(0.2) | -3.4(0.2) | -4.2(0.1) | -1.3(0.1) | | |
| $\delta_a{}^{18}O(\%)$ | -20.6(0.5) | -19.1(0.4) | -16.6(0.5) | -14.7(0.4) | -14.5(0.3) | | |
| $\delta_{\rm E}^{18}{ m O}~(\%)$ | -6.5(0.3) | -12.2(0.3) | -18.8(0.4) | -23.9(0.2) | -9.8(0.3) | | |

Table 3. Parameters used to estimate the oxygen isotopic composition of the evaporation water ($\delta_{\rm E}^{18}$ O)

The data in the parentheses referred to the standard deviation; α_K was the kinetic fractionation factor; α_{eq} was the oxygen equilibrium fractionation factor; *h* was the atmospheric relative humidity; δ_E^{18} O, δ_s^{18} O, δ_a^{18} O were the oxygen isotopic composition of evaporation water from soil surface, soil water at the evaporation surface, and air vapor, respectively

Table 4. Parameters used to estimate the oxygen isotopic composition of the evapotranspiration water ($\delta_{\rm ET}^{18}$ O)

| Damanaatama | Growth stage | | | | | | | |
|--|--------------|-------------|-------------|-------------|----------------|--|--|--|
| Parameters | Seedling | Jointing | Booting | Tasseling | Filling-mature | | | |
| Sampling date | June 24 | July 12 | July 30 | August 18 | September 20 | | | |
| $m_{\text{initial}}(\text{mm})$ | 2.50(0.08) | 2.84(0.05) | 3.57(0.11) | 2.48(0.03) | 3.22(0.07) | | | |
| $m_P(\text{mm})$ | 127.0 | 70.4 | 115.3 | 61.0 | 53.7 | | | |
| $m_{\rm final}(\rm mm)$ | 2.84(0.05) | 3.57(0.11) | 2.48(0.03) | 3.22(0.07) | 5.23(0.08) | | | |
| $m_{\rm rise}({\rm mm})$ | a | 12.23(0.26) | - | 11.24(0.14) | 71.51(0.47) | | | |
| $m_{\rm ET}(\rm mm)$ | 122.7 | 81.9 | 82.55 | 71.5 | 123.2 | | | |
| $m_{\text{infiltration}}(\text{mm})$ | 3.96(0.15) | - | 33.59(0.57) | - | - | | | |
| $\delta_{ m initial}{}^{18} m O$ | -0.5(0.1) | -0.7(0.2) | -2.4(0.2) | -3.4(0.2) | -4.2(0.1) | | | |
| $\delta_{	ext{P}}^{18}	ext{O}$ | -6.1±0.3 | -7.5±0.2 | -7.2±0.1 | -9.7±0.2 | -5.9±0.1 | | | |
| ${\delta_{\mathrm{final}}}^{18}\mathrm{O}$ | -0.7(0.2) | -2.4(0.2) | -3.4(0.2) | -4.2(0.1) | -1.3(0.1) | | | |
| $\delta_{ m rise}^{18} m O$ | - | -7.1(0.3) | - | -8.2(0.1) | -8.3(0.5) | | | |
| $\delta_{	ext{infiltration}}^{18}	ext{O}$ | -6.2(0.3) | - | -3.2(0.1) | - | - | | | |
| $\delta_{\mathrm{ET}}^{18}\mathrm{O}$ | -6.1(0.2) | -7.4(0.2) | -8.7(0.1) | -9.5(0.4) | -7.4(0.4) | | | |

^acapillary rise and infiltration couldn't be existed simultaneously; The data in the parentheses referred to the standard deviation; *m* referred to the mass of water (presented as mm) and δ^{18} O represented the oxygen isotope composition of each component. The subscripts of *initial*, *final*, *rise*, *infiltration*, *P* and *ET*, represented water in the initial soil, final soil, capillary rise, infiltration, precipitation, and evapotranspiration during each growth stage, respectively.

| Parameters | Growth stage | Total | | | | |
|--------------------------|--------------|------------|------------|------------|----------------|-------------|
| | Seedling | Jointing | Booting | Tasseling | Filling-mature | |
| δ_T^{18} O (%) | -3.1(0.1) | -4.8(0.1) | -5.9(0.2) | -6.3(0.3) | -5.0(0.1) | |
| δ_E^{-18} O (%) | -6.5(0.3) | -12.2(0.3) | -18.8(0.4) | -23.9(0.2) | -9.8(0.3) | |
| δ_{ET}^{18} O (%) | -6.1(0.2) | -7.4(0.2) | -8.7(0.1) | -9.5(0.4) | -7.4(0.4) | |
| $F_T(\%)$ | 11.8(1.5) | 65.0(5.4) | 78.3(3.0) | 81.8(5.8) | 50.0(4.3) | |
| T(mm) | 14.5(1.8) | 53.2(4.4) | 64.6(2.5) | 58.5(4.1) | 61.6(5.3) | 252.4(18.2) |
| E(mm) | 108.2.0(1.8) | 28.7(4.4) | 17.9(2.5) | 13.0(4.1) | 61.6(3.8) | 229.4(18.2) |
| <i>ET</i> (mm) | 122.7 | 81.9 | 82.5 | 71.5 | 123.2 | 481.8 |

Table 5. Parameters in isotope bass balance model during different growth stages of maize

The data in the parentheses referred to the standard deviation; $\delta_{ET}^{18}O$, $\delta_{T}^{18}O$ and $\delta_{E}^{18}O$ were the oxygen isotope composition of evapotranspiration, transpiration, and evaporation water, respectively; *ET*, T and E were evapotranspiration, maize transpiration, and soil evaporation, respectively; F_T was the fraction of plant transpiration in the field evapotranspiration.



Figure 1. Rainfall distribution and groundwater table variation during the maize growth period (from June 5 to September 12). The arrows indicated the starting date of each growth stage



Figure 2. Average soil volumetric water content at different depths during each growth stage



Figure 3. Average soil water potential at 20, 40 and 80 cmdepths during the maize growth period