# Sustainability Index for the Management of River Basins Based Upon Ecological, Environmental and Hydrological Integrity and the Minimization of Long Term Risks to Supply

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# Abstract

A new methodology for determining a sustainability index (SI) for the management of river basins is developed. Sustainability is defined in terms of minimizing the long-term risks to supply and maintaining the ecological, environmental and hydrological integrity of a river resource. The SI procedure developed uses two groups of performance criteria. The first group is based on demand-supply deficits and measures the risk to water supplies. The second group is only applied to river demands and compares a river's allocation to a target flow regime using the Range of Variability Approach (RVA) and the Modified Hydrological Alteration factor. The RVA measures differences in flow regimes and is used to compare a projected flow regime to a targeted flow regime. This is the first attempt to use the RVA to develop a sustainability index for river basin management. A combined sustainability metric for the system (SS) is also determined. The methodology is applied to an area including the Prescott Active Management Area (AMA) in north-central Arizona. Sustainability for the entire system is determined using the weighted sum of the sustainability indices. The methodology has been used to measure and compare the sustainability of two allocation scenarios for the Prescott AMA.

**Keywords:** river basin management, sustainability, range of variability approach, modified hydrologic alteration factor, sustainability index

# 1. Introduction

# 1.1 Objective

Water stress is a reality for a large portion of the world's population (Alcamo et al., 2007; Rijsberman, 2006; Rosegrant et al., 2002; Vorosmarty, 2000). Recently, the dependency of riverine ecological systems on flow regimes has been recognized (Arthington et al., 2006; Poff 2009; Poff et al., 1997) and concern over ecosystem degradation adds to the challenges of river basin management. The questions at hand are: how do managers meet immediate water demands while ensuring water availability for future needs? And, how are established societal needs balanced with the increasing awareness that human society is reliant upon a water dependent ecological system? Mays (2007) defined water resources sustainability as "the ability to use water in sufficient quantities and quality from the local to the global scale to meet the needs of humans and ecosystems for the present and the future to sustain life and to protect humans from the dangers brought about by natural and human-caused disasters that affect sustaining life."

The objective of this study is the development of a sustainability index (SI) for river basin management based upon ecological, environmental and hydrological integrity in addition to demand-supply deficit based performance criteria. The SI methodology discussed herein has been applied by Oxley, Mays, and Murray (2016) and Oxley and Mays (2016) for the optimal allocation of water for a river basin management area.

# 1.2 Sustainability for Water Resources Management

The concept of sustainability gained traction after the Brundtland Report (World Commission on Environment and Development, 1987) and discussions on definition and applications followed. In general terms, sustainability is often associated with environmental concerns, long term availability and use patterns. In this context, the concept of sustainability would seem to be especially suited to answer the water management questions raised in the

preceding paragraph. Despite the prominence and appeal of the sustainability concept, translating the current definitions and principals into practical application remains problematic (Gleick, 2000; Kuhlman & Farrington, 2010; Lant, 2007; Loucks, 1997; Loucks et al., 1999; Solow, 1993; Unver, 2007).

Applications introducing the concepts of sustainability in water resources management optimization models have been previously developed by Rothman (2007) and Rothman and Mays (2014). The use of sustainability in an optimization model for water resources planning and management was introduced by Cai (1999) and Cai et al., (2003). Sustainability in water resources can be measured using the concept of a sustainability index (SI) (Loucks, 1997; Sandoval-Solis et al., 2011; Aydin et al., 2014a and b; and Mays, 2013). These previous applications have ranged from water supply management to water distribution system sustainability to groundwater management.

Oxley, Mays, and Murray (2016) presented a new methodology for the sustainable and optimal allocation of water for a river basin management area. The model distinguishes between short and long-term planning horizons and goals using a short-term modeling component (STM) and a long-term modeling component (LTM) respectively. The STM is a linear programming problem, and optimizes a monthly allocation schedule on an annual basis in terms of maximum net economic benefit. An LTM consists of an STM for every year of the long-term planning horizon. Each LTM is quantified using a sustainability index, with the approach discussed in this paper. The LTMs are optimized to determine the most sustainable net economic benefit for the management area using a genetic algorithm. Oxley and Mays (2016) applied this model to the Prescott Active Management Area (Prescott AMA), a management area in north-central Arizona experiencing rapid population growth and limited water resources. The methodology for determining sustainability indices developed by Oxley (2015) and used in Oxley, Mays, and Murray (2016) and Oxley and Mays (2016) is described in this paper with an application to the Prescott AMA.

Sustainability requires the identification, pursuit and protection of societal objectives and ecosystem integrity. Though by no means comprehensive, societal objectives can be examined and then expressed as demands. Likewise, ecological, environmental and hydrological integrity can be expressed as demands within the system if a means of determining the demand and measuring the adequacy of both the demand and supply are available. Ecological research suggests that this is best addressed using the concept of the flow regime.

## 2. Definitions

The SI procedure developed in this research (Oxley, 2015) uses two groups of performance criteria. The first group uses demand-supply deficit based performance criteria and measures the risk to water supplies. The second group is only applied to river demands and compares a river's allocation to a target flow regime using the range of variability approach (RVA). The performance criteria are applied to a long-term allocation schedule. Sustainability for the entire system (SS) is determined using a combination of the SIs.

## 2.1 Flow Regimes

A river's flow regime is described using a record of daily flows. The target flow regime is supplied by the user. This requires a daily-flow (each 24 hours) record spanning one or more years. To ease computational burden, a monthly flow demand is determined by summing the daily flow values in the target regime for each respective month:

$$d_{j,t} = \sum_{day}^{Day} DailyFlow_{j,t,day}^{Target}$$
(1)

where  $d_{j,t}$  is the monthly demand and  $DailyFlow_{j,t,day}^{Target}$  is the daily flow value for demand node j, and day day, belonging to month t.

The projected flow regime is derived from the volume allocated to meet the river's monthly flow demand. The volume allocated, or monthly flow supplied to a river, is based upon an available monthly flow supply. To generate an available monthly flow supply, the available daily flow supply is summed over each respective month. This becomes the monthly input for a river's source node:

$$source\_input_{i,t} = \sum_{day}^{Day} DailyFlow_{i,t,day}^{Available}$$
(2)

where  $source_input_{i,t}$  is the monthly input and  $DailyFlow_{i,t,day}^{Available}$  is the daily flow value for source node *i*, and day day, belonging to month *t*. The volume at  $source_input_{i,t}$  is available for monthly allocation to a river.

After the monthly flow supply is allocated, the projected flow regime is computed by first determining the daily flow value for the projected flow regime by calculating the difference between the monthly demand and monthly supply:

$$MonthlyDifference_{j,t} = d_{j,t} - \sum_{i}^{l} x_{i,j,t}$$
(3)

where *MonthlyDifference*<sub>*i*,*t*</sub> is the difference between the demand and allocated supply,  $d_{j,t}$  is the monthly demand and  $x_{i,j,t}$  is the supply for source node *i*, demand node *j*, during month *t*. *MonthlyDifference*<sub>*i*,*t*</sub> is in turn used as the basis for determining the projected daily flows:

$$AveDailyDif_{j,t} = \frac{MonthlyDifference_{j,t}}{30.42}$$
(4)

where  $AveDailyDif_{j,t,day}$  is the average flow difference per day for demand node j, and month t. The denominator is in units of [days per year]/[months per year]. The projected daily flow is calculated as:

$$DailyFlow_{i,t,d}^{Projected} = DailyFlow_{i,t,day}^{Target} - AveDailyDif_{i,t}$$
(5)

where  $DailyFlow_{j,t,d}^{Projected}$  is the daily projected flow for demand node j, and day day, belonging to month t.

Conceptually, this is similar to a decrease in base flow for a river. The target and projected flow regimes may be compared using the RVA.

## 3. Range of Variability Approach (RVA) for Assessing Flow Regimes

Of the approaches developed for assessing flow regimes, the RVA is by far the most prevalent and widely used in the science of environmental flow assessment (Tharme, 2003). The RVA was developed in Richter et al. (1997) in response to the need to determine how much flow alteration was 'too much' and attempts to provide a comprehensive statistical characterization of ecologically relevant flow regime features.

ndex	IHA	Index	IHA
1	Median flow for month 1	17	90-day minimum
2	Median Flow for month 2	18	1-day maximum
3	Median flow for month 3	19	3-day maximum
4	Median flow for month 4	20	7-day maximum
5	Median flow for month 5	21	30-day maximum
6	Median flow for month 6	22	90-day maximum
7	Median flow for month 7	23	Number of zero days
8	Median flow for month 8	24	Base flow index
9	Median flow for month 9	25	Date of minimum
10	Median flow for month 10	26	Date of maximum
11	Median flow for month 11	27	Low pulse count
12	Median flow for month 12	28	Low pulse duration
13	1-day minimum	29	High pulse count
14	3-day minimum	30	High pulse duration
15	7-day minimum	31	Rise rate
16	30-day minimum	32	Fall rate
		33	Number of reversals

Table 1. IHA Index values used in the developed model

# 3.1 Indicators of Hydrologic Alteration (IHA)

The RVA uses the pre-impact natural variation of 33 Indicators of Hydrologic Alteration (IHA) parameter values derived from long-term daily flow records as a basis for measuring and defining the extent to which a flow regime has changed post-development (see Table 1). The IHA parameters were selected based upon two primary criteria: ecological relevance (particularly their use in published ecological studies as described by Tharme (2003)) and an ability to reflect a broad range of human induced changes. The IHAs are grouped in one of five parameter groups: magnitude of monthly water conditions; magnitude and duration of annual extreme water conditions; timing of

annual extreme water conditions; frequency and duration of high and low pulses; and rate and frequency of water condition changes (The Nature Conservancy, 2009).

To perform the RVA, flow data is separated into pre- and post-impact respective to the 'time of impact' (generally corresponding with some man-made change to the river). IHAs are independently calculated for each data set. The IHAs are further divided into three equal bins based upon either percentile values (for non-parametric analysis) or some number of standard deviations from the mean (parametric analysis), making for a total of 99 IHA parameter values. The *observed* IHA occurrences from the pre-impact period become the *expected* occurrences for the post-impact period with:

$$Expected = Observed * \left(\frac{Years^{Post}}{Years^{Pre}}\right)$$
(6)

where *Years<sup>Post</sup>* and *Years<sup>Pre</sup>* are the number of years in the post- and pre-impact datasets respectively. This process is depicted graphically in Figures 1 and 2. The change to the flow regime is expressed in terms of a series of Hydrologic Alteration (HA) factors which are calculated as:

$$HA = \frac{(Observed - Expected)}{Expected} \tag{7}$$

A positive HA value indicates an increase in the frequency of the respective IHA values from the pre- to postimpact years (maximum value of infinity), while a negative value indicates a decrease in the relative occurrences (minimum value of negative one). An HA value of zero signifies no change. A modified HA is developed and used in this research.



Figure 1. Example of non-parametric bin delineation on the pre-impact time period and expected values



Figure 2. Example of non-parametric bin assignments for the post-impact time period and observed values



Figure 3. Example modified HA values

#### 3.2 Modified Hydrologic Alteration HA

The RVA is being used in this application to compare a 'projected flow regime', which is the flow regime projected by the model, to a 'target' or ecologically sound flow regime using a Modified HA value. This concept is introduced here as performance criteria for the SI with applicable nomenclature. The 'observed' IHA values from the target flow regime become the 'expected' IHA values in the projected flow regime dependent upon the number of years being used as the basis for each regime:

$$Expected_{Bin,IHA}^{Projected} = Observed_{Bin,IHA}^{Target} * \left(\frac{Years^{Projected}}{Years^{Target}}\right)$$
(8)

where  $Expected_{Bin,IHA}^{Projected}$  refers to the IHA values for the projected flow regime;  $Observed_{Bin,IHA}^{Target}$  refers to the IHA values for the target flow regime, *Bin* is the bin index (1 through 3) (see Figures 1 and 2); *IHA* is the IHA index (1 through 33); and *Years*<sup>Projected</sup> and *Years*<sup>Target</sup> are the number of years being used as the basis for the projected and target flow regimes respectively.

As discussed previously, the IHA values for each regime are typically compared using a degree of Hydrologic Alteration (HA), reiterated here with appropriate subscripts as:

$$HA_{Bin,IHA} = \frac{\left(Observed_{Bin,IHA}^{Projected} - Expected_{Bin,IHA}^{Projected}\right)}{Expected_{Bin,IHA}^{Projected}}$$
(9)

where  $HA_{Bin,IHA}$  is the HA value,  $Observed_{Bin,IHA}^{Projected}$  is the IHA occurrence in the projected flow regime and  $Expected_{Bin,IHA}^{Projected}$  is the expected IHA occurrence for bin *Bin* and IHA index *IHA*. Values for the HA range from -1 to infinity, with 0 representing no difference between the target and projected flow regimes. It is noted that positive values signify more observed values than expected values, and for this application, it is assumed that values greater than 1 do not necessarily require more attention than the most negative value. Under this assumption, the HA has been modified  $(HA_{Bin,IHA}^{Mod})$  for this research as:

$$HA_{Bin,IHA}^{Mod} = \frac{(Observed_{Bin,IHA}^{Projected} - Expected_{Bin,IHA}^{Projected})}{(Observed_{Bin,IHA}^{Projected}} \qquad (if Expected_{Bin,IHA}^{Projected} < Observed_{Bin,IHA}^{Projected})$$

$$HA_{Bin,IHA}^{Mod} = \frac{(Observed_{Bin,IHA}^{Projected} - Expected_{Bin,IHA}^{Projected})}{(Observed_{Bin,IHA}^{Projected} - Expected_{Bin,IHA}^{Projected})} \qquad (if Expected_{Bin,IHA}^{Projected} > (1)$$

where  $HA_{Bin,IHA}^{Mod}$  is the Modified HA value,  $Observed_{Bin,IHA}^{Projected}$  is the IHA value in the projected flow regime and  $Expected_{Bin,IHA}^{Projected}$  is the IHA value in the projected flow regime for bin *Bin* and IHA index *IHA*.  $HA_{Bin,IHA}^{Mod}$  ranges from -1 to 1, with 0 still representative of no differences between the target and projected flow regimes.

#### 3.3 Interpretation of the Modified IHA

The following summarizes how the Modified HA is calculated and how the output may be interpreted. As discussed previously, the Modified HA is measuring the observed occurrences of an IHA value (projected flow) against the expected occurrences of an IHA value (target flow) and that zero signifies no difference between the projected and target flows.

Recalling the adopted terminology, the target flow regime refers to the river's demand, or the ecologically sound (assumed) flow regime; while the projected flow regime refers to the flow regime that is a result of the volume allocated to the river. A negative value indicates that the occurrences in the target flow (*Expected*) are more than the occurrences in the projected flow (*Observed*). A positive value indicates that the occurrences in the target flow (*Expected*) are flow (*Expected*) are flow (*Observed*).

As indicated earlier, the RVA preserves extreme IHA values by distributing the values among three bins. The bins are defined using the range of IHA values discovered in the target flow, the range is divided equally into three bins, and each of the IHA occurrences are assigned accordingly. As an example, consider the Median Flow in

April IHA. Assume that the Median Flow in April ranges from 18 cfs to 41 cfs in the target flow. The bin thresholds would be established as:

$$Thresholds = 29.5 [cfs] \pm 23 [cfs] * 0.17$$
(11)

where 29.5 is the median value, 23 cfs is the range, and 17% is one-half of 33% (rounded up). The assignments are as:

$$\begin{aligned} \text{Median Flow in April} &< 25.6 [cfs] = Bin 1 \\ 25.6 [cfs] &\leq \text{Median Flow in April} \leq 33.4 [cfs] = Bin 2 \end{aligned} \tag{2}$$
$$\begin{aligned} \text{Median Flow in April} &> 33.4 [cfs] = Bin 3 \end{aligned}$$

Each occurrence of the Median Flow in April in the target flow is assigned to a bin, which then become the *Expected* value of occurrences. Each value of the median flow in April discovered in the projected flow is assigned to a bin (using the same thresholds), and becomes one of the *Observed* occurrences. When *Expected* occurrences are more than the *Observed* occurrences, the  $HA_{Bin,IHA}^{Mod}$  will be negative. When *Observed* occurrences are more than *Expected* occurrences, the value of  $HA_{Bin,IHA}^{Mod}$  will be positive. General characterizations of the projected flow are listed in Table 2.

Table 2. General characterizations of the projected flow using the modified HA.

Bin	Value	Cause	Observation	Practical Interpretation
1	Positive	Observed > Expected	The projected flow has more IHAs with lower values	IHAs in projected flow tend to be lower than target flow IHAs
I	Negative	Observed < Expected	The projected flow has fewer IHAs with lower values	IHAs in the projected flow tend to be higher than target flow IHAs
ſ	Positive	Observed > Expected	The projected flow has more IHAs with median values	-
2	Negative	Observed < Expected	The projected flow has fewer IHAs with median values	-
2	Positive	Observed > Expected	The projected flow has more IHAs with higher values	IHAs in projected flow tend to be higher than target flow IHAs
3	Negative	Observed < Expected	The projected flow has fewer IHAs with higher values	IHAs in the projected flow tend to be lower than target flow IHAs

The application in this research uses an annual daily schedule of flows for the target flow. A single year of daily flows produces only one value for each of the IHA metrics. In this case, the Bins have a threshold of the discovered value  $\pm 0$ . Understanding this permits an interpretation of the sample Modified HA data presented in Figure 3. For example, the median flow in January has a modified HA value of -0.4 in Bin 2. This suggests that the median flow in January in the projected flow was not the median flow in January value discovered in the target flow. It does not however suggest that the median flow in January is smaller in magnitude in the modeled value than in the target flow. To discover this, the Modified HA value of approximately 0.17. This indicates that the median flow in January of approximately 0.35 while Bin 3 has a value of approximately 0.17. This indicates that the median flow in January value occurs more frequently in Bin 1 than it does in Bin 3. As the denominator remains the same (*Observed* > *Expected*), it can be said that the frequency of occurrence in Bin 1 is twice that of Bin 3; or that the Median Flow in January for the modeled flow is less than the value in the target flow twice as often as it is higher; suggesting a deficit in January for most of the modeled flow regime. The same method may be applied to the remaining IHAs for a general characterization of the deficiencies in the projected flow regime.

The prior discussion is unique to the one-year target regime. In practical application, a target regime encompassing several years of daily flows would allow more variance  $HA_{Bin,IHA}^{Mod}$  in the projected flows by widening the bin delineations. The following discussion uses the as a set of performance criteria in the SI.

#### 4. Computation of Sustainability Index (SI)

#### 4.1 Sustainability Index (SI)

Sustainability can be measured by the sustainability index SI:

$$SI_{g,j} = \left[\prod_{m}^{M} C_{g,m,j}\right]^{1/M}$$
(13)

where  $C_{g,m,j}$  is performance criterion *m* belonging to sustainability group *g* and demand *j*. As described, the SI ranges from 0 to 1 with a value of 1 indicating maximum sustainability.

The performance criteria in this application are divided into two groups. The first group measures the risk associated with a demand's supply and is based on demand-supply deficits. The second group measures the integrity of a river's regime and uses the Modified HA ( $HA_{Bin,IHA}^{Mod}$ ). Each demand is assigned to a sustainability group (g) based upon performance criteria applicability. For example, flow regime criteria are not applicable to non-river flow demands.

## 4.2 Demand-Supply Deficit

Demands in sustainability group 1 (g = 1) are assessed with the demand-supply deficit based criteria:

$$Def_{j,t} = d_{j,t} - \sum_{i}^{l} x_{i,j,t}$$
(14)

where  $Def_{j,t}$  is the deficit and  $d_{j,t}$  is the demand for source j in month t; and  $x_{i,j,t}$  is the volume water supplied demand for source i, demand j in month t. Deficits are positive when a demand is not fully realized for the  $j^{th}$  demand and equal to zero when the water supplied is equal to the demand  $(\sum_{i}^{I} x_{i,j,t} = d_{j,t})$ . The deficit based performance criteria are calculated over the length of the long-term time horizon for each demand and include reliability, resilience, maximum vulnerability, and maximum deficit.

#### 4.3 Reliability, Resilience, Vulnerability, and Maximum Deficit

Reliability is concerned with the number of times a demand has been fully supplied. Reliability for demand j and month t is defined as:

$$C_{1,1,j} = Rel_j = \frac{\# of \ times \ Def_{y,j,t}=0}{T}$$
(15)

where T is the total number of months.

Resilience is a measure of system recovery after a failure to meet demand:

$$C_{1,2,j} = Res_j = \frac{\# of \ times \ Def_{j,t} = 0 \ follows \ Def_{j,t} > 0}{No.of \ times \ Def_{j,t} > 0 \ occurred}$$
(16)

Maximum vulnerability is defined as the most severe of the system's failures to meet monthly demand:

$$C_{1,3,j} = MaxVul_j = Max_j \left(\frac{(\Sigma_t Def_{j,t})/\# of times Def_{j,t} > 0 occurred}{\Sigma_t x_{j,t}}\right)$$
(17)

The last performance criterion is concerned with the maximum deficit, which is defined as the most severe case of failure to meet demand:

$$C_{1,4,j} = MaxD_j = Max_j \left(\frac{\sum_t Def_{j,t}}{\sum_t d_{j,t}}\right)$$
(18)

For demands in the system that are susceptible to demand-supply deficits (g = 1), the SI is expressed as:

$$SI_{1,j} = \left[Rel_j * Res_j * \left(1 - MaxVul_j\right) * \left(1 - MaxD_j\right)\right]^{1/4}$$
<sup>(19)</sup>

The second set of performance criteria (g = 2) is based upon the differences between a target and projected flow regime as measured by the Modified HA. The SI calculation associated with these criteria is conditional based upon the value of the Modified HA:

$$SI_{2,j} = \prod_{IHA} \prod_{Bin} \left[ \left( 1 - HA_{j,IHA,Bin}^{Mod} \right) \right]^{1/99} \qquad HA_{j,IHA,Bin}^{Mod} \ge 0$$

$$\prod_{IHA} \prod_{Bin} \left[ \left( 1 + HA_{j,IHA,Bin}^{Mod} \right) \right]^{1/99} \qquad HA_{j,IHA,Bin}^{Mod} < 0$$
(3)

## 5. System Sustainability

The sustainability of a system (SS) is calculated as the sum of the weighted sustainability indexes:

$$SS = \sum_{g} \sum_{i} v_{g,i} * SI_{g,i} \tag{21}$$

where  $v_{g,j}$  is the relative weight for the *j*th water user in sustainability group *g* and ranges from zero to one and sums to one:

$$\sum_{g} \sum_{i} v_{g,i} = 1 \tag{22}$$

The potential weighting options include 1) a weighting based on water demand; 2) and arithmetic average or equalattribute-based weighting system; 3) explicit weights based on a) utility theory analysis, principal components analysis, or hedonic model according to regression coefficients; or b) based on expert and professional opinion. Determining which of these is case dependent and subjective. Principal component analysis determines weighting based on the variance of the SI, this invokes the normality assumption of theoretical statistics and utilizes the overall variance of the data matrix. The hedonic approach regresses upon variables against selected instrumental variable(s) and weights the variables per the regression coefficients (Slottje 1991).

## 6. Application of Approach to Prescott Active Management Area (AMA)

Application of the methodology was performed using the Prescott Active Management Area (AMA) in northcentral Arizona (see Figure 4). The Arizona AMAs are a management concept pursuant to the 1980 Arizona Groundwater Management Code, created to address severe ground water overdraft within the state. Five AMAs were established in Arizona, covering the areas of most severe overdraft with boundaries generally determined by groundwater basins and sub-basins (Arizona Department of Water Resources (n.d.).

## 6.1 Description of Study Area

The largest municipality in the Prescott AMA is the Town of Prescott, which is located in central Arizona and home to approximately forty-thousand people (U.S. Census Bureau 2010). The populations of Prescott and the surrounding area have enjoyed rapid growth over the last several years as more people become aware of the many benefits of residing in the area. As is often the case, rapid growth has placed undue pressure on the surrounding ecosystem and available natural resources that support the population, most notably, on the very limited water supply. In response to declining aquifer levels and regulatory compliance deadlines, the Town of Prescott AMA (see Figure 4) and AMA regulation. This plan has generated a lot of controversy as the ecological and economic impacts of the pumping are beginning to be understood. A recent study completed by the United States Geological Survey (USGS) (Pool et al., 2011) suggests that pumping in the proposed location would significantly impact the flows of the Verde River, a primary source of water for the City of Phoenix.

#### 6.2 Scenarios

Two population growth and consumption rate scenarios (see Tables 3 and 4) for the Prescott AMA are simulated and impacts to the sustainability of the system are compared as an example application. A schematic of the physical system and adaptation for the application is presented in Figure 5 with demand and source-node labels indicated in Tables 5 and 6. Each of the sources for the zones are described as independent source nodes with independent links for each source to the demand within the model but are pictured as composites in the schematic. Demand and supply are expressed for each month (t) for 50 years (T = 600). Residential demand is calculated as a linear function of consumption rate and residential population (consumers) and fulfilled at the expense of other demands in the system. Agricultural and industrial demands are assumed to be static. As demand is supplied from available source nodes, supply at the source changes as:

$$s_{i,t} = s_{i,t-1} - \sum_{j} x_{i,j,t}$$
(23)

Where  $s_{i,t}$  is the supply available at source node *i* during month *t*, and  $x_{i,j,t}$  is the volume supplied from source node *i*, to demand node *j* during month *t*. Physical parameters for the scenarios include initial residential population, population growth and consumption rates, aquifer storage levels, historical river flow data, a linear aquifer response function and infrastructure capacities.

Historical daily flow data is used as the Verde River supply basis and projected demands. Daily flows are summed to determine a monthly flow and monthly deficits are used as the basis for an average daily deficit. River supply is modified by an aquifer response function:

$$x_{9,16,t} = source_{input_{9,t}} - 0.0104 * \Delta s_{1,t}$$
(24)

Where  $x_{9,16,t}$  is the allocated supply from source node 9 (Verde River source), demand node 16 (Verde River), source<sub>input 9,t</sub> is the monthly input at source node 9 (Verde River source) based on the historical flow data and  $\Delta s_{1,t}$  is the change in storage at source node 1 (Big Chino), for month t. The coefficient is in units of month<sup>-1</sup>

and based upon data derived from an area groundwater model (Pool et al., 2011). The change in storage at source node 1 (Big Chino) is defined as:

$$\Delta s_{1,t} = s_{1,0} - s_{1,t} \tag{25}$$

where  $s_{1,0}$  is the initial storage volume and  $s_{1,t}$  is the storage volume for source node 1 (Big Chino) and month t.

A comparison of the SS values for each of the scenarios is presented in Table 7 with the demand-based performance criteria (g = 1). SI values for each demand node is depicted in Figure 6. Scenario 2 has a slightly higher value of SS, suggesting that this scenario is more sustainable than Scenario 1. Both scenarios see decreased sustainability on demand nodes 6 and 11 (Zone 1 – Chino Valley agricultural and industrial demands respectively) and a minimum SI on the Verde River (demand node 16). Figure 7 shows the ratio of annual supply to demand on the Verde River in percent.

The ratio of monthly demand and supply for the Verde River is indicated in Figure 8 with the modified HA values reflected in Figures 8 and 9. Scenario 2 sees a slightly higher fill rate on the river and less impact to median flow in June.



Figure 4. Verde watershed and relative location of the Prescott AMA



Figure 5. Schematic of the Prescott AMA



Figure 6. Demand-supply deficit based SI values for each of the demand nodes for the Prescott AMA scenarios



Figure 7. Ratio of annual supply to demand on the Verde River in percent



Figure 8. Modified HA values for Scenario 1.



Figure 9. Modified HA values for Scenario 2

Table 3. Residential	po	pulation	growth	rates	for 1	the	Prescott	AMA	scenarios
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_			Demand		
Scenario	Zone 1 - Town of Chino Valley	Zone 2- City of Prescott	Zone 3 - Town of Prescott Valley	Zone 4 - Towns of Dewey/Humboldt	Zone 5 - Unincorporated areas
1	-0.5%	0.6%	1.8%	1.6%	1.1%
2	-0.4%	0.1%	1.4%	1.3%	0.9%

Table 4. Residential consumption rates for the Prescott AMA scenarios.

			Demand		
_	Zone 1 - Town of	Zone 2- City of	Zone 3 - Town of	Zone 4 - Towns of	Zone 5 -
Scenario	Chino Valley	Prescott	Prescott Valley	Dewey/Humboldt	Unincorporated areas
_	[Ac-ft	[Ac-ft	[Ac-ft	[Ac-ft	[Ac-ft
	month/consumer]	month/consumer]	month/consumer]	month/consumer]	month/consumer]
1	8.446E-03	8.654E-03	9.572E-03	9.582E-03	9.228E-03
2	8.386E-03	8.108E-03	9.418E-03	9.168E-03	8.324E-03

## Table 5. Demand nodes for the Prescott AMA simulation

Demand Node	Label
1	Zone 1 - Town of Chino Valley
2	Zone 2- City of Prescott
3	Zone 3 - Town of Prescott Valley
4	Zone 4 - Towns of Dewey/Humboldt
5	Zone 5 - Unincorporated areas
6	Zone 1 - Agri
7	Zone 2 - Agri
8	Zone 3 - Agri
9	Zone 4 - Agri
10	Zone 5 - Agri
11	Zone 1 - Industrial
12	Zone 2 - Industrial
13	Zone 3 - Industrial
14	Zone 4 - Industrial
15	Zone 5 - Industrial
16	Verde River

Table 6. Source nodes for the Prescott AMA simulation

Source Node	Label
1	Big Chino Water Ranch
2	Zone 2 - Ground Water
3	Zone 3 - Ground Water
4	Zone 4 - Ground Water
5	Zone 5 - Ground Water
6	Zone 2 - Surface water
7	Zone 2 - Effluent
8	Zone 3 - Effluent
9	Big Chino River Source

Table 7. SS values for the Prescott AMA scenarios

Scenario	SS
1	8.4029E-01
2	8.5906E-01

## 7. Conclusions

Sustainability in this research is defined in terms of minimizing the long-term risks to supply and maintaining the ecological, environmental and hydrological integrity of a river resource. It is measured using a sustainability index comprised of two groups of performance criteria. The first group of performance criteria is based on demand-supply deficits and provides metrics for the risk to water supplies. The second group addresses the integrity of a flow regime using the RVA and Modified HA to compare a projected flow regime to a target flow regime. Sustainability for the entire system is determined using the weighted sum of the sustainability indices. The framework has been-applied to measure and compare the sustainability of two allocation scenarios for the Prescott AMA. This framework has applicability to other river basins that have the required input data.

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